

## Direct Conversion of Methane into Methanol and Formaldehyde in an RF Plasma Environment I: A Preliminary Study

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### ABSTRACT

The direct conversion of methane (CH<sub>4</sub>) into methanol (CH<sub>3</sub>OH) and HCHO in an Argon (Ar) 50W radio-frequency plasma system was applied and the effects of various feed compositions, CH<sub>4</sub>/O<sub>2</sub> ratio, and plasma discharge areas were compared. Additionally, the effects of various methane to oxygen ratios and plasma discharge areas were studied. It was found that in an Ar stream, the CH<sub>3</sub>OH conversion ratio in the CH<sub>4</sub>/O<sub>2</sub> plasma system was higher than that in CH<sub>4</sub>/CO, CO/H<sub>2</sub> and CH<sub>4</sub>/H<sub>2</sub>/O<sub>2</sub> plasma systems. The conversion of CH<sub>4</sub> reached 19.1% at CH<sub>4</sub>/O<sub>2</sub> = 40/60; the yield of CH<sub>3</sub>OH was 1.12% and 16.0% CO, the major product, was produced. A larger plasma discharge area, resulting in a longer residence time, corresponded to higher CH<sub>4</sub> conversion, but a lower CH<sub>3</sub>OH conversion ratio, because of further decomposition into CO and CO<sub>2</sub>. Interestingly, no carbon deposition was observed in the RF plasma system, and the carbon balance was between 0.94 and 1.19.

**Keywords:** Methane, methanol, formaldehyde, radio-frequency plasma

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## INTRODUCTION

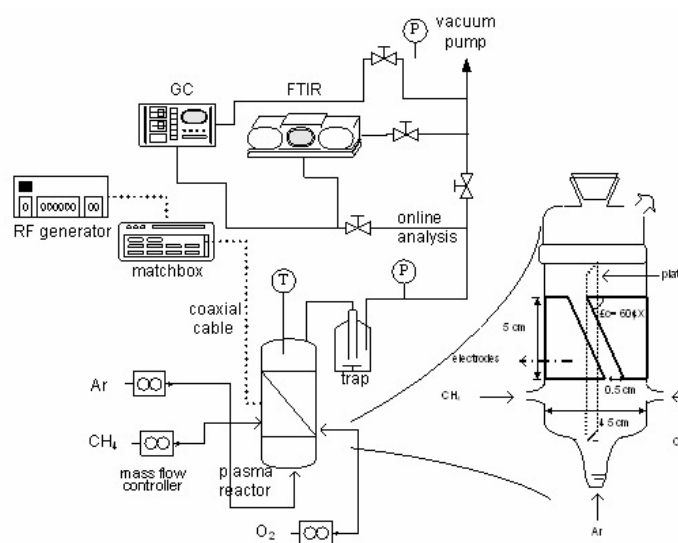
Methane (CH<sub>4</sub>) is a major contributor to the human-caused greenhouse effect. Much attention has been paid to the conversion of methane into higher hydrocarbons and easily transportable liquids, such as methanol (CH<sub>3</sub>OH) and formaldehyde (HCHO). It is expected that methane will become increasingly important in the production of energy and chemicals during this century (Roth, 1994; Brown and Parkyns, 1991). Of all available direct conversion processes, the partial oxidation of methane into useful oxygenates has great potential and is considered to be one of the greatest challenges for catalysis (Gesser, *et al.* 1985; Crabtree, 1985; Krylov, 1993).

Direct conversion technology could significantly impact the realization of more efficient energy, conserving resources and protecting the atmosphere by reducing the concentration of exhausted greenhouse gas. The difficulty in the direct conversion of methane, both catalytically and thermally, concerns the high stability of the C-H bond in the methane molecule, which exceeds that in all other hydrocarbons (Lunsford, 2000). Catalytic methods of methane conversion must eliminate the need for high reaction temperatures and the poisoning of catalysts (Lodeng *et al.*, 1995). Accordingly, the direct synthesis of methanol from methane can support a new synthetic process that consumes much less energy.

Nonthermal plasma has been used recently to excite small, stable molecules, using energetic electrons and no heating of gases. Energetic electrons are generated using either a corona, a pulse discharge, a microwave discharge, or a dielectric-barrier discharge (Suib *et al.* 1993; Liu *et al.* 1999; Huang *et al.* 2000). The products of methane conversion obtained using nonthermal plasma are mainly ethylene, acetylene, hydrogen, carbon monoxide, carbon dioxide, and some oxygenates. Some of results have led to the formation of carbon black and plasma polymerized carbon film. Very few studies have used a radio-frequency (RF) plasma system to examine the direct conversion of methane into a useful liquid fuel. In this work, the direct conversion of methane into methanol in an RF plasma system was applied and the effects of various feed compositions were compared. Additionally, the effects of various methane to oxygen ratios and plasma discharge areas were studied.

## METHODS

Figure 1 illustrates the RF plasma reactor used and schematically depicts the experiment's setup. Reactants CH<sub>4</sub>/CO/Ar, CO/H<sub>2</sub>/Ar, CH<sub>4</sub>/O<sub>2</sub>/Ar, and CH<sub>4</sub>/O<sub>2</sub>/H<sub>2</sub>/Ar were metered using Brooks Type 5850E mass flow controllers at a total flow of 100 cm<sup>3</sup>.min<sup>-1</sup>. They were then separately introduced into the reactor (4.5 cm I.D. × 15 cm height). The inside of the reactor was separated into two sections by a



**Fig 1.** Sketch of the RF plasma system

glass plate to dissociate the input gases individually and then recombine them in the effluent of the reactor. This particular reactor design was intended to improve the possibility of recombining free radicals and prevent the decomposition of  $\text{CH}_3\text{OH}$  in the reactor once it was formed. A plasma generator (PFG 600 RF, Fritz Huttering Elektronik GmbH) at 13.56 MHz, with a matching unit (Matchbox PFM), produced the RF plasma discharge. The pressure of the system had to be adjusted to under 0.0013 mbar before the experiments were performed to eliminate background contamination. Reactants and final products were first identified by gas chromatography (HP5890A); then all species were identified and their concentrations quantified using an on-line Fourier Transform Infrared (FTIR) Spectrometer (Thermo Nicolet AVATRA 360).

FTIR quantification data were obtained through a carbon balance to evaluate the significance of both deposition and condensation in the sampling and analyzing apparatus.

$$CB = \frac{\sum_{i=1}^n [(C_{out})_i \times (N_i)]}{[CH_4]_f}$$

$\text{CH}_4$  was partially oxidized at 13.3 mbar and 50W. The conversion of  $\text{CH}_4$  ( $X_{\text{CH}_4}$ ) and fraction of total input carbon converted into  $\text{CH}_3\text{OH}$  ( $F_{\text{CH}_3\text{OH}}$ ),  $\text{HCHO}$  ( $F_{\text{HCHO}}$ ) and  $\text{C}_2\text{H}_2 + \text{C}_2\text{H}_4 + \text{C}_2\text{H}_6$  ( $F_{\text{C}_2}$ ) were calculated as,

$$X_{\text{CH}_4} = \frac{[CH_4]_c}{[CH_4]_f} \times 100\% \quad (1)$$

$$F_{CH_3OH} = \frac{[CH_3OH]_p}{[CH_4]_f} \times 100\% \quad (2)$$

$$F_{HCHO} = \frac{[HCHO]_p}{[CH_4]_f} \times 100\% \quad (3)$$

$$F_{C_2} = \frac{[C_2H_2 + C_2H_4 + C_2H_6]_p \times 2}{[CH_4]_f} \times 100\% \quad (4)$$

$(C_{out})_i$  is the concentration of species *i* in the effluent (%)

$N_i$  is the number of carbon atoms in the chemical formula for species *i* in the effluent

*n* is the total number of species in the effluent

$[CH_4]_f$  is the  $CH_4$  feeding concentration (%)

$[CH_4]_c$  is the amount of  $CH_4$  consumed (%)

$[CH_3OH]_p$  is the amount of  $CH_3OH$  produced (%)

$[HCHO]_p$  is the amount of  $HCHO$  produced (%)

$[C_2H_2 + C_2H_4 + C_2H_6]_p$  is the amount of  $C_2H_2 + C_2H_4 + C_2H_6$  produced (%).

## RESULTS AND DISCUSSION

### SYNTHESIS OF METHANOL AND FORMALDEHYDE FOR VARIOUS FEED COMPOSITIONS

Table 1 shows  $X_{CH_4}$ ,  $F_{CH_3OH}$ ,  $F_{HCHO}$  and by-products in various RF plasma systems ( $CH_4/CO/Ar$ ,  $CO/H_2/Ar$ ,  $CH_4/O_2/Ar$ , and  $CH_4/O_2/H_2/Ar$ ), as well as the ratio of the various reactants. The experimental conditions were: 50W applied power; 13.3 mbar operational pressure, and  $100 \text{ cm}^3 \cdot \text{min}^{-1}$  total flow. The combination of reactants affects the patterns of the by-products in the effluent.  $X_{CH_4}$  was present in the least amount and no  $CH_3OH$  or  $HCHO$  was formed in the  $CO/H_2/Ar$  system. Only  $CO_2$ ,  $CH_4$  and  $H_2O$  were produced in the  $CO/H_2/Ar$  system. In contrast, more by-products— $CO$ ,  $CO_2$ ,  $CH_3OH$ ,  $HCHO$ ,  $C_2H_2$ ,  $C_2H_4$ ,  $C_2H_6$ ,  $H_2O$  and  $H_2$ —were detected in the  $CH_4/CO/Ar$  and  $CH_4/O_2/Ar$  system. Interestingly, neither  $HCHO$ , nor hydrocarbons were detected in the  $CH_4/O_2/H_2/Ar$  system.  $F_{CH_3OH}$  was the most present (0.96%) in the  $CH_4/O_2/Ar$  system, with a  $CH_4/O_2$  ratio of 30/60. Increasing the  $CH_4/O_2$  ratio to 30/7 reduced the  $F_{CH_3OH}$  in all except the  $CH_4/CO/Ar$  system. Based on these results, the  $CH_4/O_2/Ar$  combination was chosen in the following experiment.

**Table 1.** The reaction combination of different reactants.

ratio	CH <sub>4</sub> /CO/Ar		CO/H <sub>2</sub> /Ar		CH <sub>4</sub> /O <sub>2</sub> /Ar		CH <sub>4</sub> /O <sub>2</sub> /H <sub>2</sub> /Ar	
	30/60/10	30/7/63	30/60/10	30/7/63	30/60/10	30/7/63	30/30/30/10	30/7/7/46
X <sub>CH<sub>4</sub></sub> (%)	15.2	11.3	3.55	5.04	20.9	14.3	26.6	17.2
F <sub>CH<sub>3</sub>OH</sub> (%)	0.05	0.07	0.00	0.00	0.96	0.14	0.50	0.07
By-products	CO <sub>2</sub> , CH <sub>3</sub> OH, HCHO, C <sub>2</sub> H <sub>2</sub> , C <sub>2</sub> H <sub>4</sub> , C <sub>2</sub> H <sub>6</sub> , H <sub>2</sub> , H <sub>2</sub> O		CH <sub>4</sub> · CO <sub>2</sub>		CO <sub>2</sub> , CO, CH <sub>3</sub> OH, HCHO, C <sub>2</sub> H <sub>2</sub> , C <sub>2</sub> H <sub>4</sub> , C <sub>2</sub> H <sub>6</sub> , H <sub>2</sub> , H <sub>2</sub> O		CO <sub>2</sub> , CO, CH <sub>3</sub> OH, H <sub>2</sub> O	

## METHANOL AND FORMALDEHYDE SYNTHESIS WITH VARIOUS CH<sub>4</sub> TO O<sub>2</sub> RATIOS

Table 2 presents the effect of a CH<sub>4</sub>/O<sub>2</sub> feeding concentration on the conversion of CH<sub>4</sub>. Pure CH<sub>4</sub> has typically been regarded as rather chemically inactive, but easily decomposes in the RF plasma system. Unlike in other studies (Matsumoto, *et al.* 2001), X<sub>CH<sub>4</sub></sub> was less than 12% at a 2% CH<sub>4</sub> feeding concentration, and a 50 cm<sup>3</sup>/min<sup>-1</sup> total flow rate, while X<sub>CH<sub>4</sub></sub> was about 4% with a 5.0 mL/min<sup>-1</sup> CH<sub>4</sub> flow rate (Taylor *et al.* 2000). X<sub>CH<sub>4</sub></sub> with typical solid catalysts reported by Otsuka (2001) was 0.7% to 18.5%. In the RF system, applying 50W yielded 14.8 to 38.1% CH<sub>4</sub> conversion, while in the DBD system, 100W of input power yielded 5.97% CH<sub>4</sub> conversion (Jiang *et al.* 2002). Matsumoto (2001) stated that the intensities in Ar excitation drastically declined upon the introduction of a feeding concentration of CH<sub>4</sub> of only 2% into the Ar stream, and their system exhibited a large energy transfer from excited Ar species to reactant molecules. This suggestion was extended to the RF system. X<sub>CH<sub>4</sub></sub> was higher in the RF plasma system with Ar inflow (CH<sub>4</sub>/O<sub>2</sub> at 30/60 and 50/40) than in that without (CH<sub>4</sub>/O<sub>2</sub> = 40/60, 50/50).

The highest F<sub>CH<sub>3</sub>OH</sub>, F<sub>HCHO</sub> and F<sub>C<sub>2</sub></sub> were 1.12, 11.9 and 1.56% with CH<sub>4</sub>/O<sub>2</sub> ratios equaling 40/60, 8/8 and 8/8, respectively. The highest F<sub>CO</sub> and F<sub>CO<sub>2</sub></sub> were 24.9 and 23.1% with CH<sub>4</sub>/O<sub>2</sub> ratios of 8/8 and 50/50, respectively. Interestingly, F<sub>C<sub>2</sub></sub> generally decreased as the CH<sub>4</sub> and O<sub>2</sub> feeding concentrations increased. No carbon deposition occurred in the Matsumoto *et al.* RF system, and the carbon balance was 0.97 to 1.19.

**Table 2.** The effect of CH<sub>4</sub> to O<sub>2</sub> ratio on CH<sub>4</sub> conversion.

CH <sub>4</sub> /O <sub>2</sub> ratio	X <sub>CH<sub>4</sub></sub> (%)	F <sub>CO</sub> (%)	F <sub>CO<sub>2</sub></sub> (%)	F <sub>CH<sub>3</sub>OH</sub> (%)	F <sub>HCHO</sub> (%)	F <sub>C<sub>2</sub></sub> (%)	Carbon balance
8/8	38.1	24.9	13.4	0.79	11.9	1.56	1.14
30/60	20.9	16.4	7.20	0.96	0.24	0.33	1.04
40/60	19.1	16.0	6.38	1.12	0.18	0.28	1.05
50/40	19.3	11.2	3.04	0.90	0.80	0.24	0.97
50/50	14.8	8.71	23.10	0.15	1.91	0.02	1.19

## METHANOL AND FORMALDEHYDE SYNTHESIS FOR VARIOUS PLASMA DISCHARGE AREAS

Table 3 shows the effect of the plasma discharge area on CH<sub>4</sub> conversion. Experimental conditions were [CH<sub>4</sub>]<sub>in</sub> = 8%, [O<sub>2</sub>]<sub>in</sub> = 8%, applied power = 50 W and operational pressure = 13.3 mbar. Increasing the discharge area increased the residence time thus increasing X<sub>CH<sub>4</sub></sub>. Increasing the discharge area reduced F<sub>CH<sub>3</sub>OH</sub> and F<sub>C<sub>2</sub></sub>, while F<sub>HCHO</sub> initially increased but then fell. F<sub>CO</sub> and F<sub>CO<sub>2</sub></sub>, meanwhile, increased with increased discharge area. A longer residence time favored the formation of CO and CO<sub>2</sub> as final products of the dominant reaction pathway (Matsumoto *et al.* 2001). CH<sub>3</sub>OH is oxidized into HCHO and further decomposed into CO and CO<sub>2</sub> when the residence time is increased. Therefore, a smaller discharge area favors the production of CH<sub>3</sub>OH.

Direct conversion of methane into methanol in the RF plasma system was shown to be possible, indicating a potential for extensive abatement and reuse of methane. Experiments were conducted to clarify the influence of feed composition on CH<sub>3</sub>OH formation, on CH<sub>4</sub>/O<sub>2</sub> ratio and on the plasma discharge area. Experimental results revealed that the combination CH<sub>4</sub>/O<sub>2</sub>/Ar system favors a better CH<sub>3</sub>OH conversion fraction. The by-products detected in the CH<sub>4</sub>/O<sub>2</sub>/Ar plasma system were CO, CO<sub>2</sub>, CH<sub>3</sub>OH, HCHO, C<sub>2</sub>H<sub>2</sub>, C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>6</sub>, H<sub>2</sub>O and H<sub>2</sub>. For various CH<sub>4</sub>/O<sub>2</sub> ratios, the highest F<sub>CH<sub>3</sub>OH</sub>, F<sub>HCHO</sub> and F<sub>C<sub>2</sub></sub> were 1.12, 11.9 and 1.56% with CH<sub>4</sub>/O<sub>2</sub> ratios of 40/60, 8/8 and 8/8, respectively. The highest F<sub>CO</sub> and F<sub>CO<sub>2</sub></sub> were 24.9 and 23.1% with CH<sub>4</sub>/O<sub>2</sub> ratios of 8/8 and 50/50, respectively. Moreover, a larger plasma discharge area, resulting in a longer residence time, led to higher CH<sub>4</sub> conversion, but a lower CH<sub>3</sub>OH conversion ratio, owing to further decomposition into CO and CO<sub>2</sub>. Therefore, the CH<sub>4</sub>/O<sub>2</sub>/Ar plasma system of reactor A was selected as the basis for the further investigation of the effects of experimental parameters on X<sub>CH<sub>4</sub></sub>, F<sub>CH<sub>3</sub>OH</sub> and F<sub>HCHO</sub>.

**Table 3.** The effect of plasma discharge area on CH<sub>4</sub> conversion.

Discharge area (cm <sup>3</sup> )	X <sub>CH<sub>4</sub></sub> (%)	F <sub>CO</sub> (%)	F <sub>CO<sub>2</sub></sub> (%)	F <sub>CH<sub>3</sub>OH</sub> (%)	F <sub>HCHO</sub> (%)	F <sub>C<sub>2</sub></sub> (%)	Carbon balance
A (320)	38.1	24.9	13.4	0.79	11.9	1.56	1.14
B (450)	65.2	31.6	26.2	0.42	15.3	1.47	1.10
C (1080)	88.6	35.3	38.6	0.43	6.60	1.39	0.94

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