



Efficient Adsorption of Hydrogen Sulfide at Room Temperature Using Fumed Silica-supported Deep Eutectic Solvents

Jiaming Mao¹, Yunqian Ma^{1,2*}, Lihua Zang^{1**}, Rong Xue¹, Cong Xiao³, Dandan Ji^{1,2,4}

¹ College of Environmental Science and Engineering, Qilu University of Technology (Shandong Academy of Science), Jinan 250353, China

² Jiangsu Key Laboratory of Anaerobic Biotechnology (Jiangnan University), Wuxi 214122, China

³ Shandong Huacheng Construction Design and Engineering Co., Ltd., Jinan 250301, China

⁴ Huatai Group, Guangrao 257335, China

ABSTRACT

Supported deep eutectic solvents (SDESs) using fumed silica as the supporting material and TAECuCl₃ as the loading substance, were developed for H₂S removal. The highest breakthrough sulfur capacity, 9.97 mg g⁻¹, was achieved when the molar ratio of the TEACl to the CuCl₂ was 1:1, the loading rate of the DES was 10%, and the temperature was 30°C. TAECuCl₃ proved to be a more effective loading substance than pure TEACl, pure CuCl₂, or blends of these substances at other ratios. Due to the high utilization rates of the metal-activated sites, the SDESs were more economical. The excellent capacity for H₂S removal was attributable to the formation of a thin layer of DES, nano-sized in thickness, on the fumed silica. The XRD and XPS analysis showed that the products of desulfurization were S and Cu₂S, the latter of which was then oxidized to S and SO₄²⁻ by air at room temperature. After regenerating 4 times, the breakthrough sulfur capacity of the SDESs was still as high as 7.39 mg g⁻¹. The nonlinear curve fitting demonstrated that the adsorption kinetics followed those of the Bangham kinetic model.

Keywords: Hydrogen sulfide; Adsorption; Fumed silica; Deep eutectic solvents.

INTRODUCTION

It is well known that hydrogen sulfide (H₂S) and other sulfur-containing compounds found in industrially important hydrocarbon feedstock have severe negative impact on human beings and the ecosystem in general (Montes *et al.*, 2013). These sulfuric compounds can increase corrosion in process equipment, and lead to the deactivation of catalysts and environmental threat in end-use upon combustion (Liu and Wang, 2017; Ma *et al.*, 2017). H₂S can cause various respiratory symptoms, even death at a low level (10–500 ppmv) (Yang *et al.*, 2006). Up to now, many technologies such as gas-liquid absorption, adsorption or biological process are used to remove H₂S. Nevertheless, the gas-liquid absorption process with an aqueous solution of ammonia, alkanolamine or alkaline salts suffers from the drawbacks of foaming,

inapplicability for high temperature and requiring high energy consumption for the regeneration (Ma and Wang, 2014a). Although biological process could efficiently remove H₂S, it costs much time and is inefficient with H₂S of high concentration. Adsorption by metal oxides, activated carbon, zeolite or silica which is recognized to be an efficient technology for H₂S removal at high temperature, but requires a stable support with a high adsorption capacity and selectivity towards H₂S gas.

In order to solve the aforementioned drawbacks, ionic liquids (ILs) have been widely studied for H₂S absorption and oxidation due to their extremely low vapor pressures, high thermostability, and tunable chemical structures (Welton, 1999; Fukumoto *et al.*, 2005). In wet desulfurization, the wide interest in ILs arises from a general need for environmentally friendly, new green solvents to replace water, which present the problem of high volatility at high temperature (Liu and Wang, 2016). Especially, enhanced absorption of H₂S into functionalized ILs, such as amino-based, metal-based (Ma and Wang, 2014b), substituted benzoate-based and pyridinium-based ILs (Huang *et al.*, 2016a), is an attractive approach that exhibits benign H₂S removal capacities. However, the drawbacks of these ILs, such as high viscosity, complicated synthesis and high costs, may limit their large-scale application. The viscosity of H₂S-absorbed IL is very high resulting in

* Corresponding author.

Tel.: +86 531 89631680; Fax: +86 531 89631680

E-mail address: yqma_1986@163.com

** Corresponding author.

Tel.: +86 531 89631680; Fax: +86 531 89631680

E-mail address: ZLH@qlu.edu.cn

long absorption equilibrium time (Huang *et al.*, 2016b; Xue *et al.*, 2018). The chemical industry for gas separation still prefers gas-liquid systems with low viscosity or gas-solid systems due to the ease of operation and the economic criteria; it is desirable to minimize the amount of utilized ILs in an industrial process. Wang *et al.* (2019) found that (bmim)TF₂N is a potential ionic liquid that can remove both H₂S and CO₂, with a CO₂ removal rate of 97.6% and H₂S removal rate of 95.3%, and can save a lot of refrigeration energy. However, it can not meet the requirements of gas refining, and its application is still limited. Ge *et al.* (2019) developed a new polyfiber ionic liquid with good adsorption capacity of H₂S at room temperature, up to 1.75 mmol L⁻¹, but its breakthrough sulfur capacity was low, 0.92 mmol L⁻¹, and it could not be used for sulfur recovery.

To take advantage of IL properties while avoiding their negative aspects, on the one hand, supported ionic liquid or ionic liquid combined system could overcome the shortcomings of ionic liquids (Wang *et al.*, 2016; Xue *et al.*, 2018), such as, high cost, high viscosity, and cut the amount of utilized ILs, but the complex synthesis of ionic liquid must proceed, and most solvents in the combined system are toxic; on the other hand, a new type of solvents, deep eutectic solvents (DESs), are emerging as versatile alternatives to ILs that provide similar features. DESs have benign characteristics such as comparatively low cost, low toxicity, high biodegradability and accessible synthesis (Smith *et al.*, 2014; Azizi and Edrisi, 2017). DESs could be obtained by simply mixing the hydrogen bond donor (HBD; such as metal chloride) and hydrogen bond acceptor (HBA; such as quaternary ammonium halide salt) by heating and stirring, without additional purification operations, leading to a significant depression of the freezing point (Gorke *et al.*, 2008; Dai *et al.*, 2013; Smith *et al.*, 2014; Azizi and Edrisi, 2017). Although DESs which is regarded as another class of IL variants have been successfully applied in different research fields, few of them have been reported for H₂S removal, and some functional DESs of high viscosity are inadaptable for gas separation as a liquid-phase absorbent (Smith *et al.*, 2014). They have been rarely reported for H₂S removal. Liu *et al.* (2019a) has studied four kinds of metal-based low transition temperature mixtures, which were synthesized by metal chlorides and choline chlorides, and the results were satisfactory. Furthermore, supported DESs (SDESs) have a promising application in H₂S removal, on the one hand to minimize the unfavorable sides for ionic liquid gas-liquid system and the use of DESs, and on the other side to improve the utilization rate of DESs (Huang *et al.*, 2019).

Considering these facts and inspired by the early work of our groups in DESs systems (Ma *et al.*, 2019a), we became

interested in the immobilization of DESs onto silica materials. Herein, fumed silica (FS) was selected as the supported materials because of the specific performance characteristics, high chemical stability and low cost (Liu and Maciel, 1996; Liu *et al.*, 2019b), Si-OH from FS could enhance the cation and anion interaction to stabilize DESs in the space more firmly (Qian *et al.*, 2018). The main aim of this work is to optimize the ratio of HBA and HBD of the DES, and test the H₂S removal efficiency of DESs immobilized on fumed silica prepared by simply physical immobilization. The H₂S removal mechanism and regeneration performance were evaluated.

MATERIALS AND METHODS

Materials

H₂S (99.999%) and N₂ (99.999%) were supplied by Jinan Deyang Special Gas Co., Ltd. (Shandong, China). Triethylamine hydrochloride (TAECI; 99 wt%), cupric chloride (CuCl₂; 99 wt%) and iron trichloride (FeCl₃; 99 wt%) was purchased from Shanghai Macklin Biochemical Co., Ltd. Fumed silica was purchased from Sunny Chemicals (H.K.) Ltd. Carbon disulfide (CS₂; metal basis, 99.99 wt%) was purchased from Sinopharm Chemical Reagent Co., Ltd. The TH-990S portable smoke analyzer was purchased from Wuhan Tianhong Instrument Group and the D08-1F flow indicators were provided from Beijing Sevenstar Electronics Co., Ltd. All the chemicals were used directly without further purification.

Preparation of DESs and SDESs

TAECI and CuCl₂ were used as HBA and HBD of the DES, respectively. 13.76 g of TAECI was mixed with 13.44 g of CuCl₂ (molar ratio is 1:1) and the mixture were heated to 70°C under stirring in inert atmosphere for 24 h, and finally DES TAECuCl₃ was obtained. The other DESs with different molar ratio of TAECI and CuCl₂ were synthesized using the same method. The DES product is a thick black-brown liquid at 70°C, but semisolid at room temperature.

The SDESs was achieved via inverse supported approach (Kazuya *et al.*, 2005) without complicated synthetic modification. Firstly, the high-viscosity DES of certain amount was dissolved in 70 mL mixed solvents (the volume ratio of acetonitrile to ethanol is 3:1). Then, FS was added to the above mixture, and treated with ultrasound at 120 W for 10 min. The solvents were then evaporated at reduced pressure, and the resulting mixture was finally dried for 24 h at 60°C in vacuum. The illustration of molar ratios and loading amount was listed in Table 1.

Table 1. The notes and molar ratios of samples.

Ratios ^a	0.6:1	0.8:1	1:1	1.2:1	1.4:1	1.6:1	1.8:1
DESs	TAE _{0.6} CuCl _{2.6}	TAE _{0.8} CuCl _{0.8}	TAECuCl ₃	TAE _{1.2} CuCl _{3.2}	TAE _{1.4} CuCl _{3.4}	TAE _{1.6} CuCl _{3.6}	TAE _{1.8} CuCl _{3.8}
Notes	TAE _x CuCl _y @FS/z wt% ^b						

^a the molar ratios of TAECI and CuCl₂ (TAECI:CuCl₂).

^b x and y represent the molar ratio of TAECI to CuCl₂ in DESs, respectively. And z wt% represents the amount of DESs immobilized on fumed silica.

Desulfurization Test

The desulfurization test was carried out using two quartz tubes (inner diameter of 6 mm and height of 10 cm) connected in series with silicone hose. 0.5 g of sorbent (the length of sorbents layer were 60 mm) was packed into each tube and the desulfurization temperature was controlled by thermostat water bath. A gas mixture (nitrogen as the carrier gas) containing 800 ppm (1231 mg L⁻¹ at standard condition) of H₂S was passed through the sorbent at a flow rate of 100 mL min⁻¹. The H₂S concentration of the outlet gas was detected by a TH-990S hydrogen sulfide gas analyzer. The residual H₂S gas was absorbed by NaOH solution before discharging into the atmosphere. The H₂S removal efficiency of the desulfurizer was calculated by Eq. (1). C_{in} and C_{out} are the inlet and outlet concentration of H₂S (mg m⁻³), respectively (Liu et al., 2019a).

$$H_2S \text{ removal efficiency (\%)} = \frac{C_{in} - C_{out}}{C_{in}} \times 100\% \quad (1)$$

The breakthrough curve was expressed as a plot of the outlet concentration of H₂S versus time. In addition, the breakthrough sulfur capacity (S_{cap}) was calculated using Eq. (2) when the outlet concentration of H₂S was higher than 20 mg m⁻³ (Shen et al., 2018).

$$S_{cap} = \frac{M_S}{M_{H_2S}} \times \frac{Q_{H_2S}}{m} \left[\int_0^t (C_{in} - C_{out}) dt \right] \times 10^{-6} \quad (2)$$

where S_{cap} represents the breakthrough sulfur capacity of sorbents; M_S and M_{H_2S} are the molar weight (g mol⁻¹) of S and H₂S, respectively; m is the weight of sorbents; Q_{H_2S} is the H₂S gas flow rate; t is the reaction time (min) for desulfurization.

In order to measure the efficiency of the unit adsorbent (ω), we calculated the molar ratio of metal ions to absorbed H₂S. The formula was shown in Eq. (3) (Nath and Yadav, 2018):

$$\omega = \frac{n_{H_2S}}{n_{Cu}} \quad (3)$$

Characterization

The Fourier transform infrared spectroscopy of materials were studied using FT-IR spectrophotometer (IRAffinity-1S; Shimadzu, Japan). The surface morphologies of materials were obtained by scanning electron microscopy (SEM; Regulus8220; Hitachi, Japan). The element composition and valence state of materials were obtained by X-ray photoelectron spectroscopy with multifunctional imaging electron spectrometer (Thermo Scientific ESCALAB 250 XI; Thermo Fisher, USA). The specific surface area of materials was determined by the BET (Brunauer-Emmett-Teller) and the pore size distribution was calculated by the BJH (Barrett-Joyner-Halenda) from the isotherm of adsorption branch with automatic specific surface area and porosity analyzer

(TriStar II 3020; Micromeritics, USA).

RESULTS AND DISCUSSION

Characterization of DESs and SDESs

Fourier Transform Infrared Spectrometer

The inverse supported method is simple and easy without complicated synthetic modification on FS. It is just a process of physical deposition, therefore, the characteristics of the sorbent depend solely on the DESs and FS (Jaiboon et al., 2014). The FT-IR spectrum of SDESs were shown in Fig. 1. Due to the small amount of solid load, the adsorbents maintains the infrared characteristics of FS itself. The peak at 798 cm⁻¹ is the symmetric stretching vibration peak of Si-O, and the peak at 958 cm⁻¹ was attributed to the structure of Si-OH. The peak at 1095 cm⁻¹ was attributed to Si-O-Si anti-scale vibration peak. At last, the broad peak at 3429 cm⁻¹ was belong to the -OH of H₂O, which may come from the air during the process of sample preparation (Cheng et al., 2019).

Surface Area and Porosity Analysis

The N₂ adsorption-desorption isotherms of FS and TAECuCl₃@FS/10 wt% were shown in Figs. 2(a) and 2(b). The typical Type IV isotherms with H4 characteristics loop were obtained. There are some mesoporous, slit pores and inter-particle pores (mainly macropores) in both samples. The DES was well dispersed in the mesopores of the silica material and the FS kept its original structure after the loading of DES (Jaiboon et al., 2014). The surface area and pore volumes of SDESs can be seen in Table 2. The surface area of FS (153.3172 m² g⁻¹) decreased after the deposition of DESs. The same situation was found for the pore volumes of the SDESs. The pore size distribution curve of FS before and after DESs loading was shown in Fig. 3. It can be found that the mesopores and macropores were dominant before and after the deposition of DESs, and there were a few micropores.

With the increase of the loading amount, the specific surface area of FS decreased, while the pore width increased. This showed that with the increase of the loading amount, a large number of DESs deposited on the surface of FS, leading to the reducing of the specific surface area for FS. The pore volume increased first and then decreased, because with the increase of loading amount, the micropores and mesopores are filled out by DESs first, and then the excessive loading could lead to the deformation of the surface structure or collapse (Widiana et al., 2019). Although the loading substance DES can improve the removal ability of H₂S by FS, it should be emphasized that the high specific surface and pore volume also plays the important roles in the adsorption of H₂S. In particular, mesoporous plays a more important role in catalytic oxidation (Soriano et al., 2009; Sun et al., 2013; Kwok et al., 2017; Wang et al., 2018; Li et al., 2019).

Surface Morphology Analysis

The SEM image of the samples was shown in Figs. 4(a)–4(e). There were many pores on the surface of the original fumed silica in Fig. 4(a). With the increase of loading amount

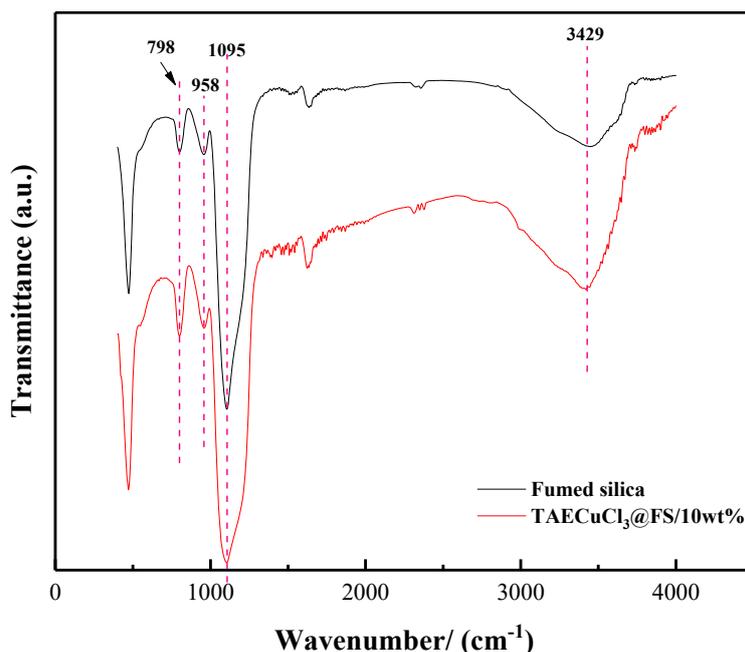


Fig. 1. FT-IR spectra of FS and SDEs (TAECuCl₂@FS/10 wt%).

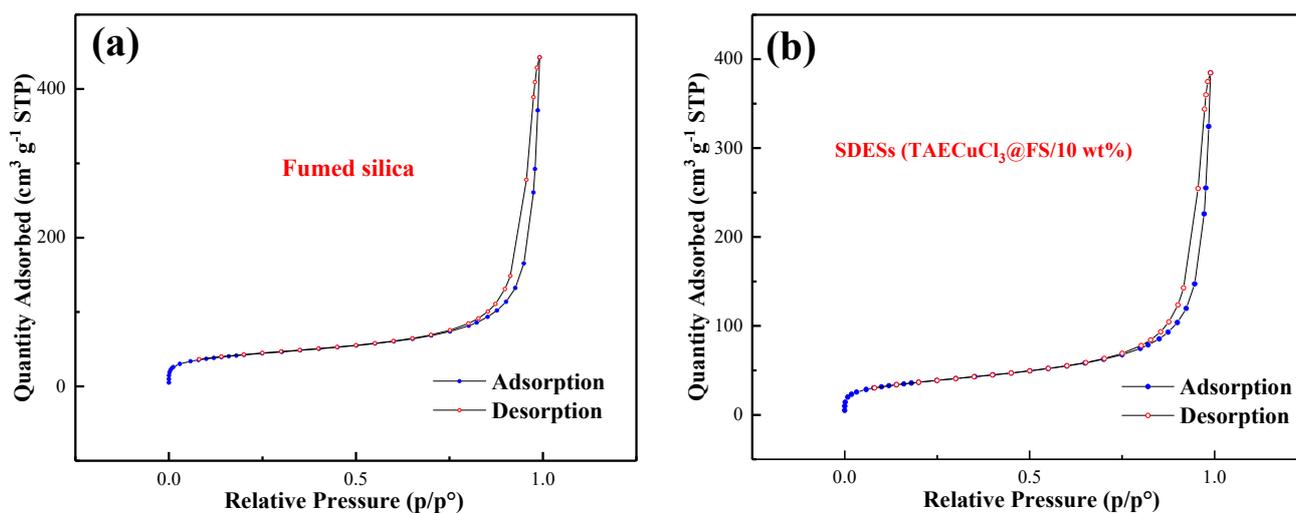


Fig. 2. Curves of nitrogen adsorption-desorption of (a) FS and (b) TAECuCl₃@FS/10 wt%.

Table 2. Physical parameters of three kinds of sorbents.

Desulfurizer	Surface are (m ² g ⁻¹)	Pore width (nm)	Pore volumes (cm ³ g ⁻¹)
FS	153.3172	17.8534	0.6843
TAECuCl ₃ @FS/10 wt%	132.5190	17.9551	0.5948
TAECuCl ₃ @FS/20 wt%	124.0691	20.2953	0.6295

for DESs, the granular volume of FS surface gradually increased and the surface gradually became smooth. When its surface was deposited with 10 wt% DES in Fig. 4(b), it can be seen that the surface of FS becomes smoother and denser, indicating that DESs has a nice and stable load on the surface FS. It could be found that there was still a developed mesoporous structure on the surface of FS, which

ensured the catalysis and adsorption properties of the material itself. The successful incorporation of DESs into the fumed silica framework can be identified and estimated by EDS elemental mapping of Cu, and the result was shown in Figs. 4(d) and 4(e). The blue dots in the figure represent the Cu elements distributed on the surface of FS. Cu in the structure of nano-composite can be further confirmed.

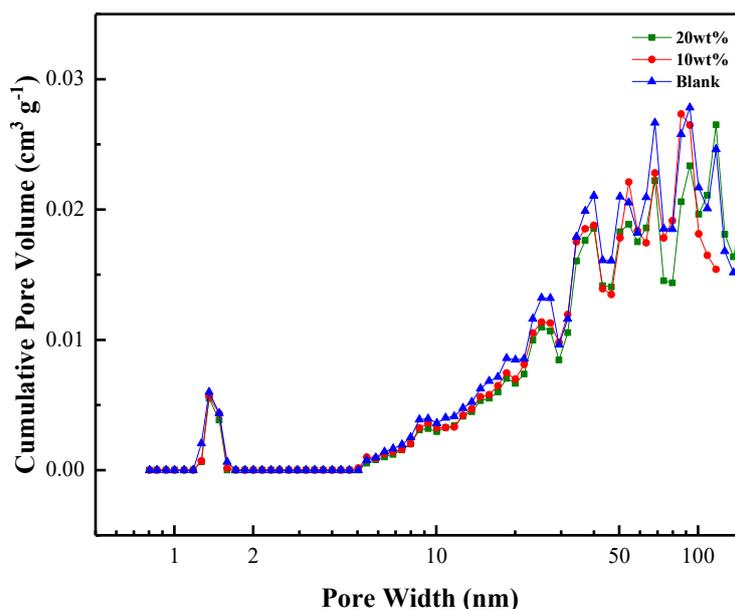


Fig. 3. The pore diameter distribution curves of the materials.

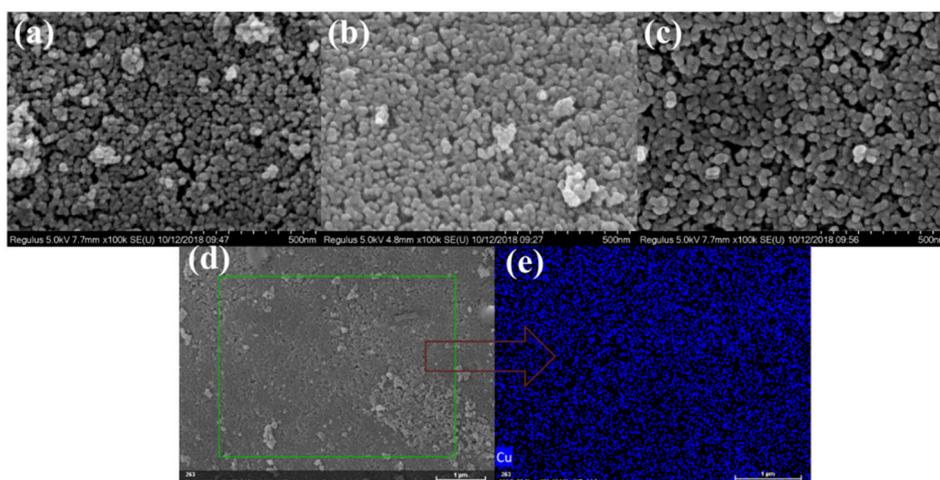


Fig. 4. The SEM images of FS and SDESs. (a) Fumed silica without DESs, (b) TAECuCl₃@FS/10 wt%, (c) TAECuCl₃@FS/20 wt%, and (d, e) EDS elemental mapping of Cu before adsorption.

Similar to room-temperature ionic liquid, in pure DESs, complex grid-like hydrogen bonds will be formed between molecules (Dong *et al.*, 2006). This structure will solidify the DESs molecules, increase the viscosity of materials, prevent the H₂S molecules from entering the grid, and greatly affect the mass transfer efficiency (Lungwitz and Spange, 2008; Dong and Zhang, 2012), which results in low utilization of DESs and poor catalytic oxidation. The DESs molecules are connected by planar grid hydrogen bonds, and it is no longer a 3D grid structure, which can greatly improve the utilization rate of DESs (Shi *et al.*, 2005). When the proportion and content of immobilized DESs is appropriate, it will form a nanometer thin layer of DESs on the surface of fumed silica. Moreover, some physical and chemical properties of the DESs will change under the nanometer conditions to enhance the catalytic ability.

Determination of Optimum Conditions

Effect of Different Loading Substances on FS

In this part, we did a series of single factor experiments to determine the optimum condition (loading substances, loading amount, and desulfurization temperature) in the desulfurization system. The H₂S removal efficiency (%) and sulfur capacity (mg g⁻¹) were selected as evaluation index.

The sulfur capacities of SDESs under different molar ratios of TAECuCl₃ and CuCl₂ in DESs from 0.6:1 to 1.8:1 were tested, and the condition of desulfurization was the temperature of 30°C, loading rate of 10 wt%, and the gas flow rate of 100 mL min⁻¹. The breakthrough sulfur capacity of the SDESs were measured and showed in Figs. 5(a) and 5(b).

As it can be observed that the sulfur capacity of H₂S in TAECuCl₃@FS/10 wt% (when the molar ratio is 1:1) is higher than that of other different molar ratios of TAECuCl₃ and CuCl₂. The dynamic viscosity model of DESs under different

molar ratios was shown in Fig. 6, and the dynamic viscosity of TAECuCl_3 DESs increased sharply with the decrease or increase of molar ratio of TAECuCl_3 and CuCl_2 . Not only did it reduce the number of active sites, but also the high viscosity of the DESs limits the mass transfer of H_2S , which results in the sulfur capacity of H_2S decrease. DESs of high viscosity are easy to be agglomerated on the surface of fumed silica. In addition, Cu^{2+} is used as oxidant and complexing agent, and TAECuCl_3 is used as the activator of hydrogen sulfide molecule. The increase or decrease of its mixture ratio will make the activated HS^- surplus and premature overflow, which is not conducive to fine desulfurization (Chatterjee et al., 2018).

Original FS, $\text{TAECuCl}_3@FS/5$ wt% and $\text{CuCl}_2@FS/5$ wt% were first studied. Since there is little difference between TAECuCl_3 and CuCl_2 on the relative molecular mass, $\text{TAECuCl}_3@FS/10$ wt% can be regarded as $\text{TAECuCl}_3@FS/5$ wt% and $\text{CuCl}_2@FS/5$ wt%. It can be seen from the data that the breakthrough time of original FS was 174 seconds (not shown in the figure), and its desulfurization capacity is weak due to its pore structure and physical adsorption. The desulfurization ability of $\text{TAECuCl}_3@FS/5$ wt% is slightly weaker than that of original FS, its breakthrough time was

132 seconds (not shown in the figure). Because the pore structure is the important factor rather than amino adsorption by TAECuCl_3 , and the deposition of TAECuCl_3 on FS blocks the pores and does not benefit to adsorption of H_2S . Although $\text{CuCl}_2@FS/5$ wt% has higher desulfurization capacity and longer breakthrough time, it is still weaker than $\text{TAECuCl}_3@FS/10$ wt% and cannot be regenerated.

Effect of Different Loading Amount of TAECuCl_3 on FS

To confirm the best loading amount, SDES with different loading amount of TAECuCl_3 was tested for H_2S removal, and the results are shown in Figs. 7(a) and 7(b). H_2S removal efficiency of SDESs increased as the loading amount of TAECuCl_3 increasing from 0% to 20%. Although high loading could lead to high sulfur capture, it was unfavorable for the dispersion of active phase in carrier material, resulting in a decline in utilization rate of active phase during desulfurization process. As the loading increasing, more microspheres in the carrier material were clogged by DESs, and the mass transfer resistance of H_2S into the pore increased, which made it difficult to fully react with the chemically active sites in SDESs. Moreover, excessive DESs can form large aggregates that

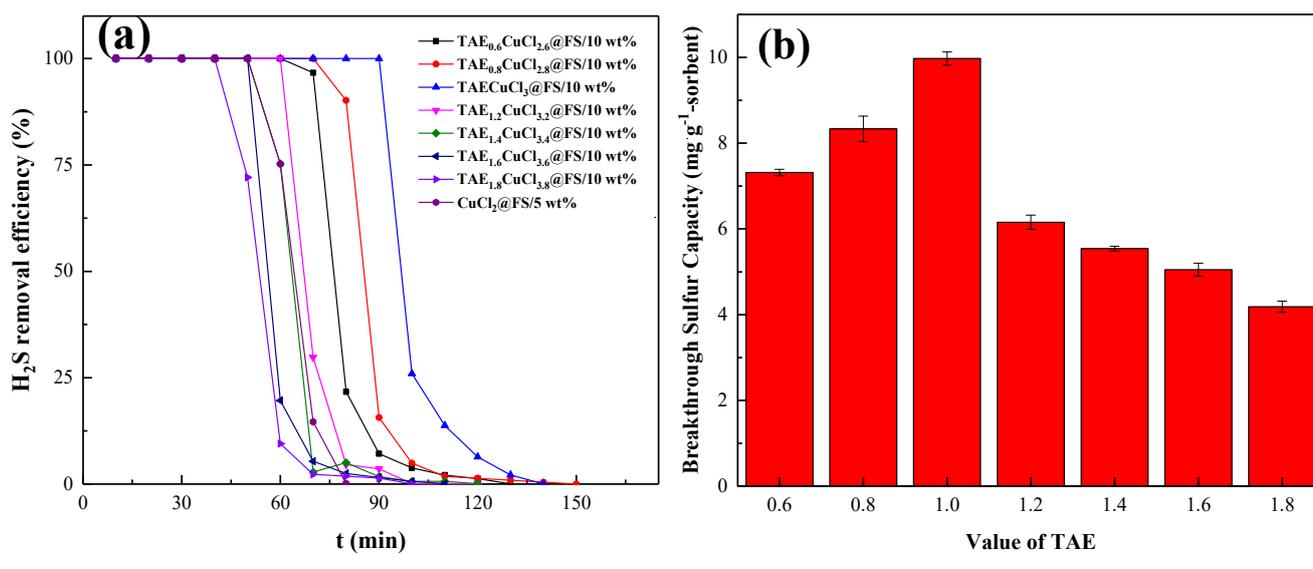


Fig. 5. (a) H_2S breakthrough sulfur curves and (b) capacity of SDESs for different molar ratios of TAECuCl_3 and CuCl_2 .

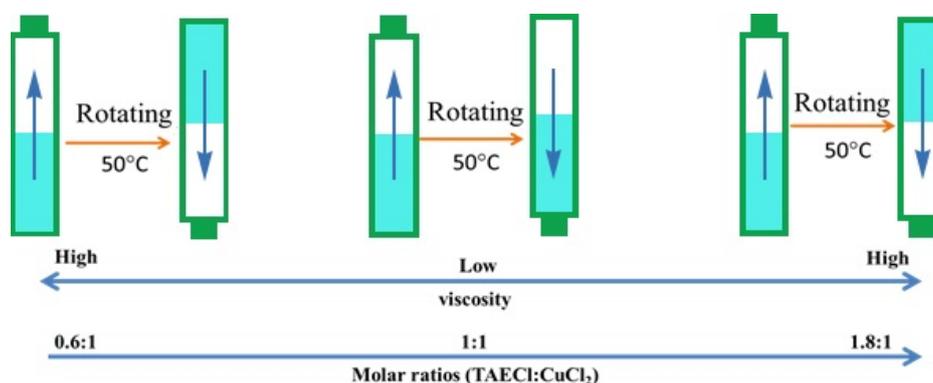


Fig. 6. The states of DESs under different molar ratios. When the molar ratio was 1:1, DESs has the lowest viscosity and melting point. With the increase or decrease of molar ratios, the viscosity and melting point was increased.

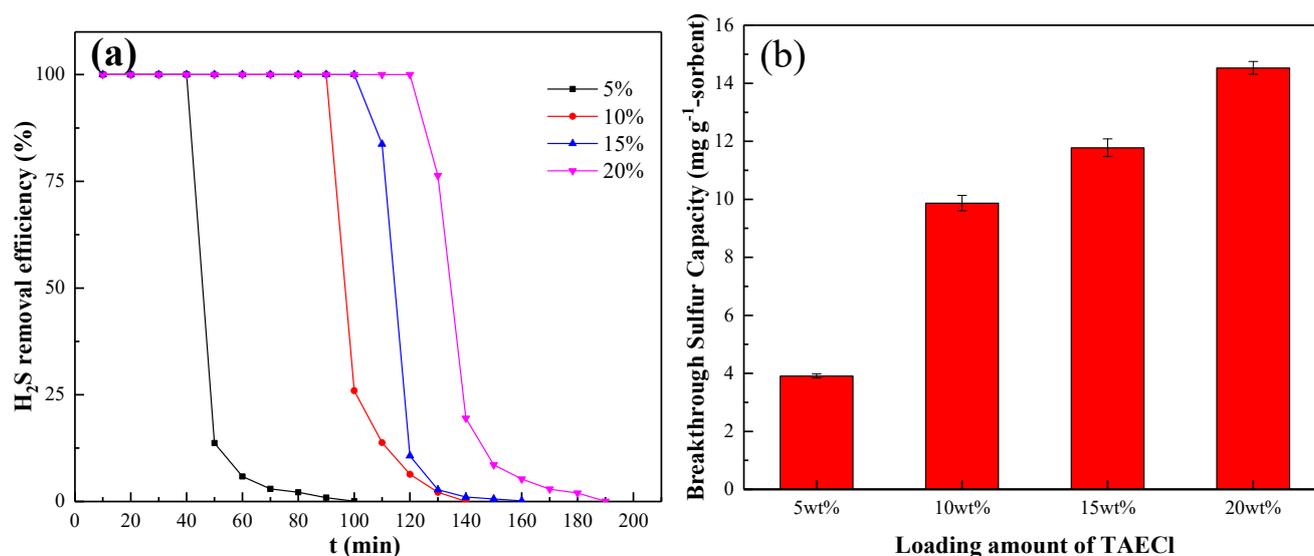


Fig. 7. (a) H₂S breakthrough curves and (b) sulfur capacity of TAECuCl₃@FS with different loading amount of TAECuCl₃.

cover the surface of FS and prevent the carrier material from exerting its effect (Ma *et al.*, 2019b). After a comprehensive consideration, the optimal content of SDESs was 10 wt%.

Here, we also studied the adsorption efficiency (ω) in Eq. (3) described above, and the value of ω reflecting the utilization rate of metal active sites is summarized in Table 3. The highest value of ω is 0.8669, it is a high level, which can be explained as follows: First, FS can interact with DES to fully reduce the size of surface DESs micro clusters and promote the transformation of metal active sites; secondly, the addition of copper can also significantly reduce the limit of solid diffusion (Balsamo *et al.*, 2016); thirdly, copper containing ZnS has a higher sulfur anion mobility, leading to a more complete reaction (Balsamo *et al.*, 2016), and copper ions in SDESs may play a similar role in this study; fourthly, in this study, dense metal sulfide layer will not be formed, so the reaction is more sufficient (Balsamo *et al.*, 2016).

Effect of Different Desulfurization Temperature

Desulfurization performance of the sorbents depended critically on temperature, which controlled S²⁻/Cu²⁺ react rate, gas diffusion efficiency, the viscosity of DESs, etc. The H₂S removal performance of SDESs in different temperature was shown in Figs. 8(a) and 8(b). It can be seen that when the temperature is over 30°C the removal efficiency of H₂S by SDESs decreases with the increase of temperature. The

breakthrough and saturation sulfur adsorption capacities of SDESs reached the maximum value at 30°C. According to previous research, this kind of absorption is an exothermal reaction (Min *et al.*, 2015). When the temperature is 20°C, the sulfur capacity is lower than 30°C, it may due to the lower temperature increases the viscosity of DESs and affects the mass transfer effect. The higher temperature can enhance the molecular mobility and interaction probability of the reactants, and hence promote the adsorption of H₂S molecular on SDESs. However, higher temperature can hinder the H₂S absorption due to exothermic reaction. According to experiment result, the low temperature (30°C) becomes the best choice for H₂S removal. The SESs has a highest breakthrough sulfur capacity in optimum condition of 9.97 mg g⁻¹ of sorbent (in Table 3).

Recycle of SDESs for H₂S Absorption

To evaluate the recyclability of SDESs for H₂S absorption, the regeneration of SDESs was carried by sweeping air directly. The temperature for regeneration is 20°C, and using the air flow rate of 50 mL min⁻¹. The SDESs is then extracted by CS₂ and dried. The decrease of its desulfurization capacity may be due to the gradual collapse of the structure and the failure to completely remove S. The regeneration performance of SDESs is shown in Fig. 9. The H₂S removal efficiency was test after 2 h of absorption, and was all above

Table 3. A desulfurization performance summary over TAECuCl₃-activated sorbents.

Absorption	S_{cap}	ω	Loading % wt	Ref.
TAECuCl ₃ @FS/5 wt%	3.87	0.6440	5	This work
TAECuCl ₃ @FS/10 wt%	9.97	0.8669	10	
TAECuCl ₃ @FS/15 wt%	12.06	0.7296	15	
TAECuCl ₃ @FS/20 wt%	14.34	0.6771	20	
TAECuCl ₃	28.98	0.2436	100	
TAECu _{0.6} Cl _{2.6} @FS/10 wt%	7.39	0.5163	10	
TAECu _{1.8} Cl _{3.8} @FS/10 wt%	4.16	0.4903	10	
TAECuCl ₃ - β -CDGZ	7.75	0.60	14	Our previous work (Ma <i>et al.</i> , 2019a)

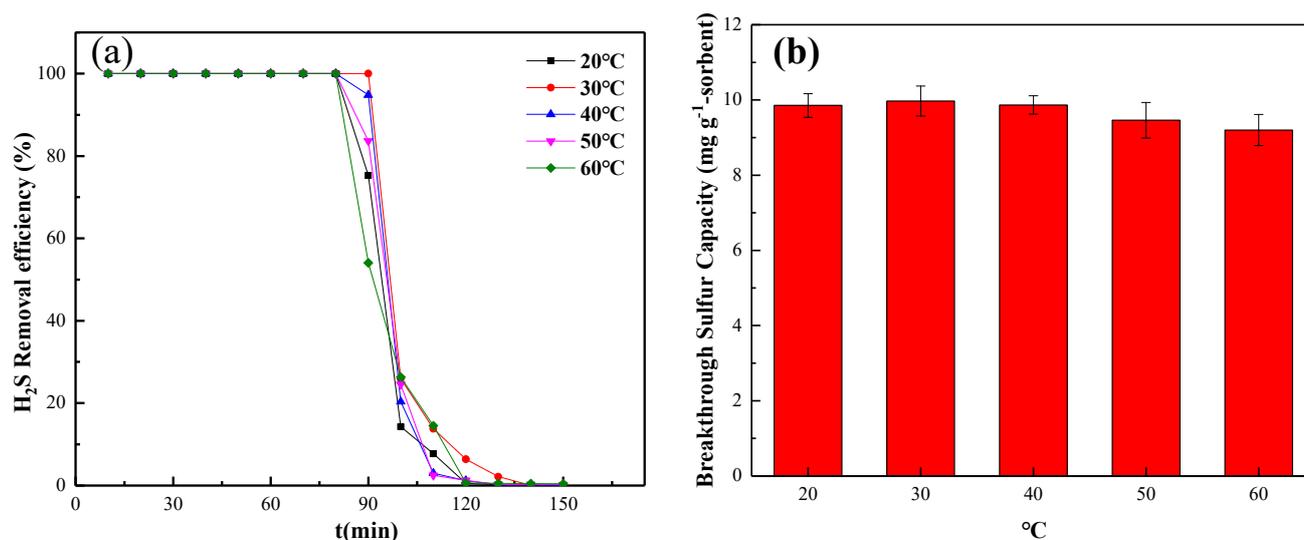


Fig. 8. (a) H₂S breakthrough curves and (b) sulfur capacity of TAECuCl₃@FS/10 wt% at different temperature.

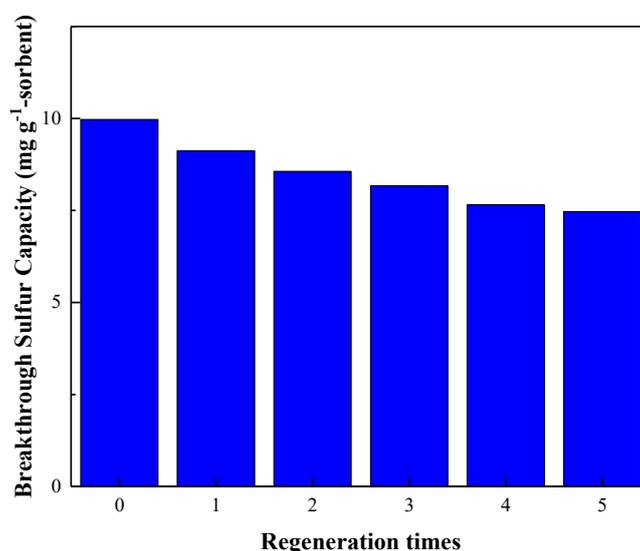


Fig. 9. Regeneration performance of TAECuCl₃@FS/10 wt%.

73% within 4 cycles, which demonstrate that the SDESs have an excellent regeneration performance in the process of H₂S removal. The color change of SDESs in the process of synthesis, adsorption and regeneration was shown in Fig. 10.

Because the recovered elemental sulfur and SDESs are both solid, it is impossible to recover elemental sulfur through simple filtration. The two possible recovery methods are as follows: Firstly, the adsorbent was extracted by CS₂, and then the elemental sulfur was obtained after removing the solvent CS₂; secondly, the H₂S-adsorbed SDES was purged with hot N₂ to separate out sublimate elemental sulfur and condense it under appropriate conditions.

Analysis of Desulfurization Products

A small amount of yellow, hard and brittle solid were obtained by vacuum evaporation of CS₂ solution containing desulfurization products at 40°C and under vacuum for 24 h. The obtained crystal was analyzed by XRD, and the results

are shown in Fig. 11. The position of the main diffraction peaks of the product is consistent with the rhombic sulfur (No. 8–247) in the JCPDS standard spectrum. Therefore, it can be determined that the desulfurization product contains a small amount of rhombic sulfur crystal. Since Cu²⁺ is more oxidizing than Fe²⁺ but weaker than Fe³⁺, the oxidation product contains a certain amount of S.

To investigate the reaction mechanism, chemical valence states of element Cu and S in TAECuCl₃@FS/10 wt% in the whole process were analyzed by XPS, and were shown in Figs. 12(a)–12(d). The XPS spectrum of S after adsorption was shown in Fig. 12(a). The valence state of S was confirmed by binding energy within the range of 162–172 eV. It showed that S(0) 2p_{3/2} appeared at 164.20 eV, and S(II) 2p_{2/3} appeared at 167.65 eV, and the binding energy position of the S 2p_{2/3} from SO₄²⁻ of sample is 169.10 eV, indicating that the valence state of S element is +6, –2 and 0 (Wagner and Taylor, 1980; de Jong *et al.*, 1993; Yu *et al.*, 1990). During the regeneration

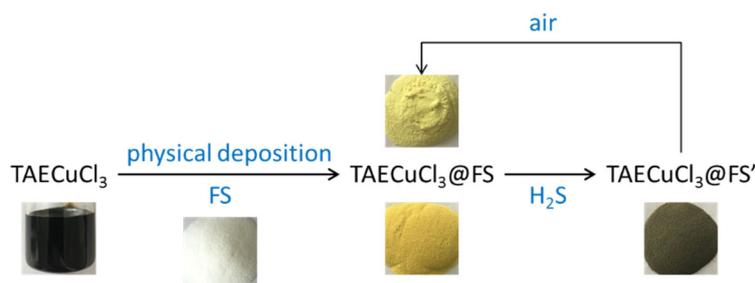


Fig. 10. The color changes of SDEs in the process of synthesis, adsorption, and regeneration.

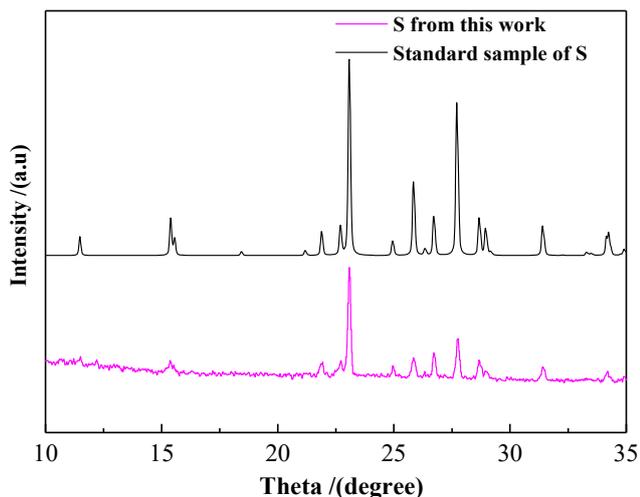


Fig. 11. XRD spectra of desulfurization products and standard rhombic sulfur.

experiment, we observed that the samples after adsorption were easy to regenerate naturally in the air. Therefore, the presence of SO_4^{2-} in the samples before regeneration may be caused by the inevitable contact with air during the XPS sample preparation process. This indicates that a small part of sulfur in H_2S gas is oxidized to sulfate ions and elemental sulfur, and most combined with copper ions to form Cu_2S . After regeneration, the result was shown in Fig. 12(c). The binding energy at 167.65 eV was disappeared, that indicated that all the sulfur in Cu_2S has been oxidized to S and SO_4^{2-} . The XPS spectrum of Cu after adsorption was shown in Fig. 12(b). The Cu^+ was confirmed by the Cu $2p_{3/2}$ binding energy within the range of 930–937 eV without any shake-up satellite peak (Jin and Nam, 2006). It shows Cu(I) $2p_{3/2}$ appeared at 932.9 eV and Cu(I) $2p_{1/2}$ appeared at 952.40 eV. It illustrates that the Cu in the adsorption exists in the form of Cu_2S after adsorption (Deroubaix and Marcus, 1992; Perry and Taylor, 1986). The XPS spectrum of Cu after regeneration was shown in Fig. 12(d). The Cu^{2+} was assigned to the binding energy of the XPS contribution ranging from 928 to 937 eV with a satellite contribution in the range of 937–947 eV (Jin and Nam, 2006; Ma et al., 2019b). Compared with the state before regeneration, Cu(I) was oxidized to Cu(II) by oxygen in air. Cu(II) $2p_{3/2}$ appears at 932.70 eV and Cu(II) $2p_{1/2}$ appears at 952.70 eV in Fig. 12(d) (Perry and Taylor, 1986).

In order to study the mechanism of the reaction more clearly, the FT-IR spectrum of TAECuCl_3 in the whole

process was tested. The result was shown in Fig. 13. For the three curves, the broad band at 3480 cm^{-1} can be assigned to the existence of N-H structure. The band at 3044 cm^{-1} is caused by hydrogen bond vibration between N-H bond in TAECl and Cl^- in CuCl_2 . The broad band at 2495 cm^{-1} can be assigned to the C-H bond in TAE (Min et al., 2015). In addition, a new peak has emerged after the absorption of H_2S at 2355 cm^{-1} , where the broad band can be assigned to the existence of S-H structure in HS^- , this is because H_2S is adsorbed in DESs, reduces the activation energy of the reaction (Ma and Wang, 2014a; Zheng et al., 2018). This kind of DESs has been synthesized successfully. The infrared spectrum of DESs after adsorption was shown in Fig. 13. The peak at 2355 cm^{-1} was disappeared, means the reactivity of DESs was loses, and H_2S cannot be adsorbed by DESs. And the peak at 3044 cm^{-1} was reduced, because the CuCl_2 in the system was converted to Cu_2S , which caused the hydrogen bond to break. Moreover, in the adsorption saturated DESs, the peak of N-H bond has a red shift, which is caused by the fact that the fracture of hydrogen bond reduces the electron cloud density and activity of N-H structure, it indicates that the two components in DESs have synergistic effect through hydrogen bond (Liu et al., 2006). DESs immobilization technology was applied in the area of H_2S removal, which improves the utilization rate and unit adsorption of DESs due to the formation of the nanometer thin layer with DESs, and also reduces the usage and cost of DESs. It can be regarded as a process of fine desulfurization, and can recover elemental sulfur. The disadvantage is that the total sulfur capacity of the adsorbent is not outstanding, and some sulfur in H_2S is converted into sulfate, which is not convenient to be recovered.

Adsorption Kinetics

In order to investigate the adsorption kinetics of H_2S on SDEs, the adsorption breakthrough curve was measured in the form of a bubbling fluidized bed. Then, four equations, pseudo-first-order, pseudo-second-order, intra-particle diffusion and Bangham models, have been tested.

The pseudo-first-order equation is expressed as Eq. (4) (Bilgili, 2006):

$$q_t = q_e[1 - \exp(-k_1t)] \quad (4)$$

where q_t and q_e are amounts of H_2S adsorbed (mg g^{-1}) at time t (min) and at equilibrium, respectively, and k_1 is the rate constant of adsorption (min^{-1}).

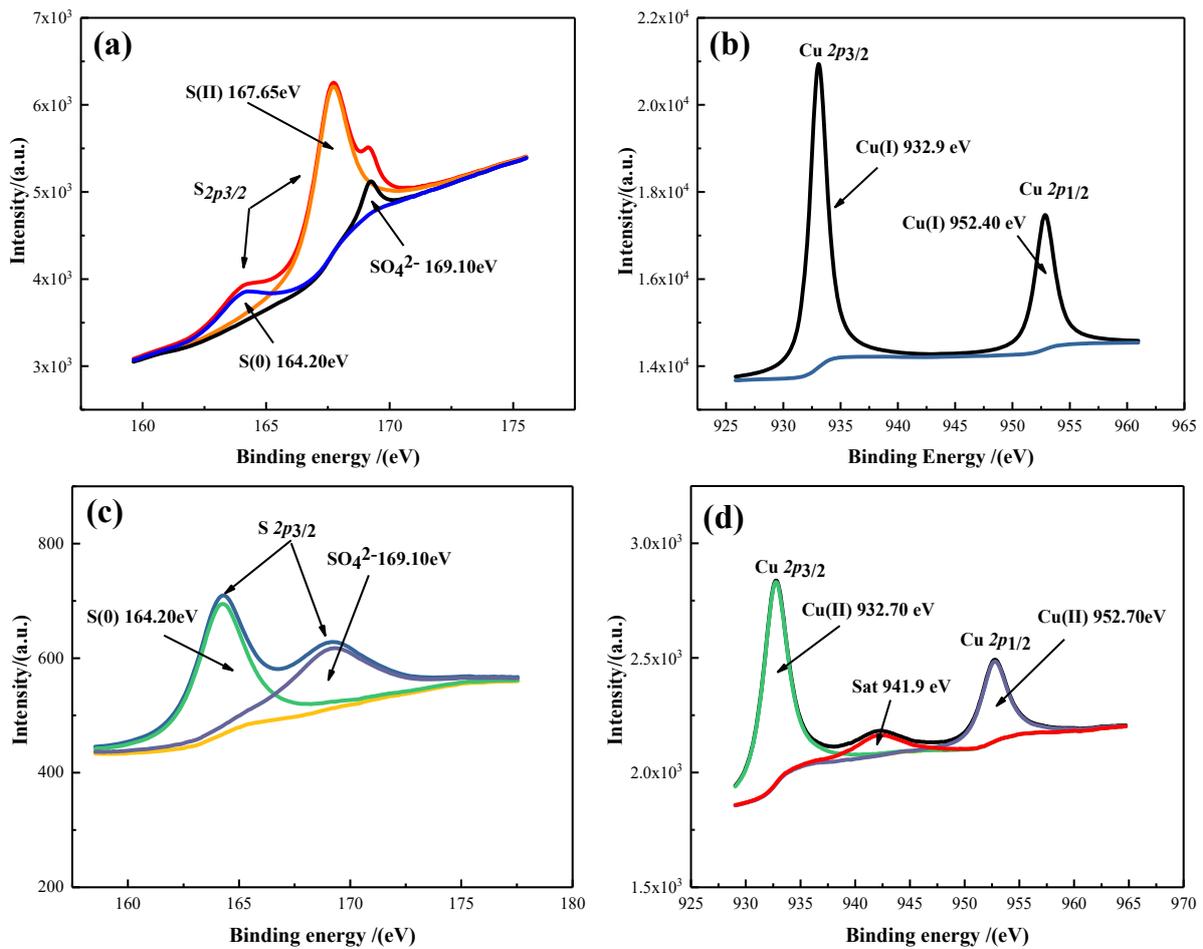


Fig. 12. XPS results for SDESs. (a) S $2p_{3/2}$ after adsorption until saturation, (b) Cu $2p_{3/2}$ and Cu $2p_{1/2}$ after adsorption until saturation, (c) S $2p_{3/2}$ after completely regeneration, and (d) Cu $2p_{3/2}$ and Cu $2p_{1/2}$ after completely regeneration. So after the first adsorption only a small amount of sulfur crystals are produced, more sulfur crystals are produced in the process of air regeneration. This prevents too much sulfur from clogging the pores during the selective oxidation process, affecting the single-adsorption effect.

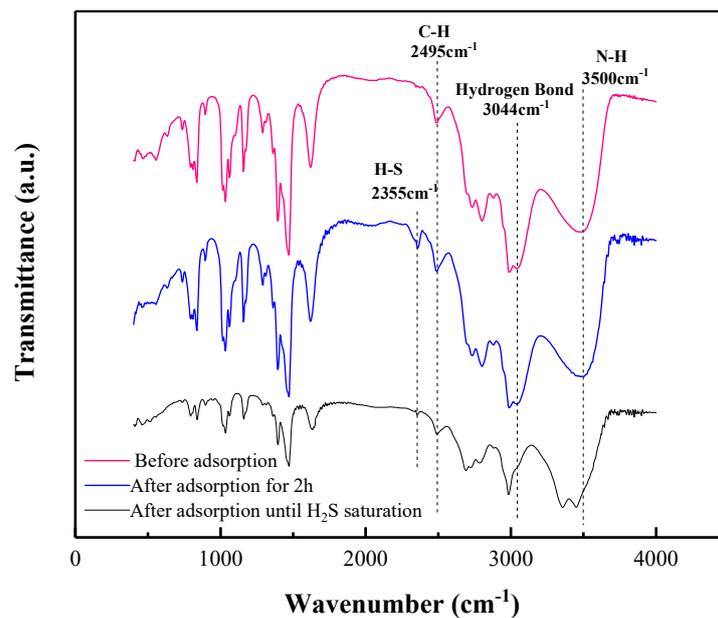


Fig. 13. FT-IR spectrum of DESs.

The pseudo-second-order equation is expressed as Eq. (5) (Bilgili, 2006):

$$q_t = k_2 q_e^2 t / (1 + k_2 q_e t) \quad (5)$$

where k_2 is the rate constant of adsorption ($\text{g mg}^{-1} \text{min}^{-1}$).

The intra-particle diffusion model can be represented as Eq. (6) (Bilgili, 2006):

$$q_t = k_i t^{0.5} + C \quad (6)$$

where k_i is the intra-particle diffusion constant ($\text{mg g}^{-1} \text{min}^{-0.5}$), and C is a constant (mg g^{-1}).

The Bangham model is expressed as Eq. (7) (Bilgili, 2006):

$$\log \log [q_e / (q_e - q_t)] = \log (k_b / 2.303) + n \log t \quad (7)$$

q_t can be written as Eq. (8):

$$q_t = q_e [1 - \exp(-k_b t^n)] \quad (8)$$

where k_b is Bangham constant, and n is constant.

The experimental data and nonlinear fitting of four kinetics models are shown in Fig. 14. TAECuCl₃@FS/10 wt% was used to be tested. The kinetics parameters and the correlation coefficients of models were listed in Table 4. As it can be seen, the Bangham model fit the adsorption data best, which demonstrate that the adsorption kinetics are limited by pore diffusion. DESs strengthened the adsorption of H₂S by pores and did not fundamentally change the adsorption mechanism (Bilgili, 2006).

CONCLUSIONS

In this research, a new kind of SDES desulfurizer was synthesized via the inverse supported approach and used to remove H₂S. The optimum desulfurization conditions were determined to be a 10% loading of DES, an operating

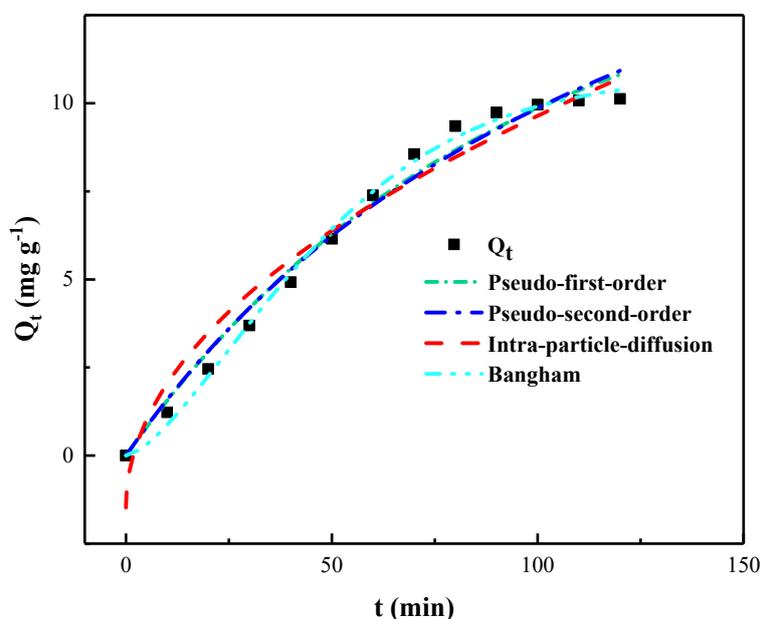


Fig. 14. Adsorption kinetics of H₂S on the optimized SDES.

Table 4. Kinetic parameters for SDESs (loading amount: 10 wt%, gas flow rate: 100 mL min⁻¹, temperature: 30°C).

Models	Parameters	Value
Pseudo-first-order	R ²	0.9850
	k ₁ (min ⁻¹)	0.01131 ± 0.00186
	q _e (mg g ⁻¹)	14.5545 ± 1.43924
Pseudo-second-order	R ²	0.9823
	k ₂ (g mg ⁻¹ min ⁻¹)	3.06805E-4 ± 1.170
	q _e (mg g ⁻¹)	23.52797 ± 3.45656
Intra-particle diffusion	R ²	0.95276
	k _i (mg g ⁻¹ min ^{-0.5})	1.11203 ± 0.07466
	C (mg g ⁻¹)	-1.4783 ± 0.5783
	R ²	0.99628
Bangham	k _b (min ⁻ⁿ)	0.00282 ± 8.92138E
	q _e (mg g ⁻¹)	10.76371 ± 0.29746
	n	1.47712 ± 0.08997

temperature of 30°C, and a molar ratio of 1:1 for the HBA to the HBD. Under these conditions, the maximum breakthrough sulfur capacity was 9.97 mg g⁻¹, whereas the maximum utilization rate of the DES was 86.69%. Furthermore, the breakthrough sulfur capacity of the SDESs following 4 regenerations still reached 7.39 mg g⁻¹. XPS and XRD analysis showed that the desulfurization products were S and Cu₂S; Cu₂S subsequently oxidized into CuSO₄ and S during the regeneration process. The nonlinear curve fitting demonstrated that the adsorption kinetics followed those of the Bangham kinetic model. The deposition of a thin layer of DES, nano-sized in thickness, on the fumed silica enabled the highly efficient removal of H₂S. Thus, SDESs can potentially be used to remove toxic gas or H₂S due to their high efficiency, high utilization rates, and economic feasibility.

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