

Technical Note

## Estimates of atmospheric aerosols adhered to the high voltage electric wire in the Yangtze River Delta region of China

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1 **Abstract.** Atmospheric aerosol particles can be collected by and adhered to high voltage  
2 electric wires and can cause the power loss as well as other detrimental effects on electrical  
3 insulation. The mass of fine particles (PM<sub>2.5</sub>) adhered to wires is estimated using a modified  
4 size-resolved particle dry deposition model and a range of annual average PM<sub>2.5</sub>  
5 concentrations found in literature in the Yangtze River Delta region of China. Annual mass  
6 collected by the surface of an unit length (1 m) of wire with a radius of 0.5 cm is estimated to  
7 be in the range of  $1.56 \times 10^4$  -  $1.46 \times 10^5$   $\mu\text{g}$ . The actual mass adhered to the wire may be  
8 reduced by 85% of these estimated values considering washed off effects by rain. For a wire  
9 of 1.0 cm in radius, the annual mass adhered to the wire is estimated to be in the range of  
10  $4.68 \times 10^3$  -  $4.35 \times 10^4$   $\mu\text{g}$  after considering the wash-off effects by rain. This study provides a  
11 first estimation of particle mass collected by electric wires, although with large uncertainties,  
12 which can be used for subsequent impact studies of aerosol pollution on electricity transfer.

13  
14 **Key words:** Dry deposition model; Electric wire; Mass of PM<sub>2.5</sub>.

## 16 **1 Introduction**

17 Mass concentrations in air of atmospheric aerosol particles have been at high levels across  
18 China (Tao et al., 2017) in the most recent decades due to increasing energy consumption  
19 (Wang et al., 2016; Ma et al., 2017) and rapid economic growth (Liu et al., 2016; Sun et al.,  
20 2017; He et al., 2017). Increased aerosol air concentrations can enhanced particle deposition  
21 amounts to any surfaces including high voltage electric wires with the power loss. In  
22 particular, particle deposition on insulator can decrease flashover voltage and increase

23 leakage current, posing a threat to electric power supply safety (Wu et al., 2004; Zhao et al.,  
24 2007; Li et al., 2014; Hu et al., 2015). Particle deposition (marine salt, industrial and  
25 agricultural pollutants), in the presence of elevated humidity levels, greatly increase the  
26 surface conductivity of lines and substations insulators and can lead to surface discharges and  
27 electrical short-circuits. The persistence of these conditions poses a threat to the continuity of  
28 service of the electrical grid and may produce extended blackouts in large areas of the  
29 network such as the blackout phenomena due to pollution on the whole island of Sardinia,  
30 Italy (Troccoli et al. 2014).

31  
32 Some efforts have been made to simulate the impact of particle pollution on flashover  
33 incidents (Gençoğlu et al., 2008; Jiang et al., 2010), but little has been done to estimate the  
34 amount of particle mass deposition on electric wires. The purpose of the present study aims to  
35 provide a rough estimation of particle mass adhered to high-voltage electric wires in the  
36 Yangtze River Delta region of China. To do this, the size-resolved particle dry deposition  
37 model of Zhang et al. (2001) is first modified to include the effect of electric charge since this  
38 mechanism might be important in the collection of fine particles by electric wires. Modeled  
39 dry deposition velocities under typical turbulent conditions are then combined with a range of  
40 annual average PM<sub>2.5</sub> concentrations found in this region, as documented in Tao et al. (2017).  
41 Coarse particles are not considered here since they may not be adhered to the wire  
42 permanently due to blowing off effects by strong winds and washing off effects by rain.  
43 Uncertainty analyses have also been conducted to provide a range of possible values for the  
44 estimated annual particle mass adhered to different sizes of wires.

45

## 46 **2. Methodology**

47 Dry deposition flux to various land surfaces is commonly based on unit land surface area.

48 Electric wire is in cylinder shape so the particle mass adhered to electric wire is calculated

49 based on a unit length in this study with surface area as a function of wire diameter. The

50 size-resolved particle dry deposition model of Zhang et al. (2001) is modified to estimate the

51 rate of particles adhered to surface of electric wire. The collection efficiencies of particles by

52 electric wire surface are certainly different from those by land surfaces so modifications are

53 made as detailed below.

54

55 According to Zhang et al (2001), particle dry deposition velocity ( $V_d$ ) is calculated as:

$$56 \quad V_d = \frac{1}{(R_a + R_s)} \quad (1)$$

57 where  $R_a$  and  $R_s$  are aerodynamic and surface resistance, respectively. Because wire is

58 installed at high levels in the sky where winds are generally strong,  $R_a$  should be negligible in

59 most cases. A value of  $10 \text{ s}^{-1} \text{ m}$  is used throughout the study. Note that the gravitational

60 settling velocity in the original formula was excluded here considering the cylinder shaper of

61 the wire surface may not collect all the particles through this mechanism. Besides,

62 gravitational setting is a minor contributor to the deposition of fine particles (Zhang and He,

63 2014), which is the focus of the present study as further explained below.

64

65 The surface resistance is parameterized as a function of various collection mechanisms:

$$66 \quad R_s = \frac{1}{\varepsilon_0 u_* (E_B + E_{IM} + E_{IN} + E_E) R_1}, \quad (2)$$

67 where  $\varepsilon_0$  is an empirical constant (0.3),  $u^*$  is friction velocity,  $E_B$ ,  $E_{IM}$ ,  $E_{IN}$  and  $E_E$  are  
 68 collection efficiencies by Brownian diffusion, impaction, interception, and electric charge,  
 69 respectively.  $R_1$  is the factor considering particle rebound (the fraction of particles collide  
 70 with the surface and not bounced back).  $E_B$  and  $E_{IM}$  by electric wire surface are considered to  
 71 be smaller than any land surface described in Zhang et al. (2001) so the minimum values  
 72 (such as over bares soil) are used here for these two terms.  $E_{IN}$  is calculated as a function of  
 73 particle diameter and wire radius. A value of 0.5 cm is used for wire radius as the base case in  
 74 the present study based on a survey in the studied region.

75  
 76  $E_E$  is a new term added in this study, representing the collection efficiency by electric force  
 77 generated by wire on particles. According to Wang et al. (2010),  $E_E$  is parameterized as:

$$78 \quad E_E = \frac{16KC_cQq}{3\pi\mu_aVD^2d_p} \quad (3)$$

79 where  $K = 9 \times 10^9 (\text{N m}^2 \text{C}^{-2})$ ,  $C_c$  is Cunningham correction factor as a function of particle  
 80 diameter and the mean free path of air molecules,  $Q$  and  $q$  are the surface charge of high  
 81 voltage wire and particle, respectively,  $\mu_a$  is air viscosity,  $V$  is gravitational setting velocity of  
 82 particles, and  $D$  and  $d_p$  are the diameters of wire and particle, respectively.  $Q$  was expressed  
 83 as:

$$84 \quad Q = \sigma S, \quad (4)$$

85 where  $\sigma$  is surface charge density of high voltage wire and the value was taken from Jiang et  
 86 al. (2015) as  $12 \times 10^{-6} (\text{C m}^{-2})$ .  $S$  can be calculated as a product of section girth and length of  
 87 wire. Here, the length of wire was chosen as 100 times of particle size in order to generate  
 88 effective electric force between wire and any size particles.  $q$  can be calculated according to

89 Wang et al. (2010):

$$90 \quad q = a \partial d_p^2, \quad (5)$$

91 where  $a = 0.83 \times 10^{-6}$  and  $\partial (\text{C m}^{-2})$  is an empirical parameter that can vary between 0 and 7.

92 Here  $\partial$  is taken as 7 because the electric field around high voltage wire is very strong.

93

94 Particle mass deposit and adhere to a wire (M) can then be estimated as:

$$95 \quad M = C * V_d * (2\pi r L) * t \quad (6)$$

96 Where C is the mass concentration of particles in air, r is the wire radius, L is wire length, t is  
97 the time period. Considering that large particles collide with wire may not easily adhere to the  
98 wire since they can easily be blown away by strong winds or washed off by rain, only fine  
99 particles (PM<sub>2.5</sub>) are considered in Eq (6). Since particle size distribution is needed for  
100 calculating size-resolved V<sub>d</sub>, a log-normal size distribution is assumed following Zhang and  
101 He (2014) with geometric mass median diameter and geometric standard deviation chosen as  
102 0.4 μm and 2.2, respectively.

103

### 104 **3. Results**

#### 105 **3.1 Dry deposition velocity**

106 Figure 1 shows a comparison of size-resolved V<sub>d</sub> calculated using the modified and the  
107 original models with a u\* value of 0.5 m s<sup>-1</sup>. It is seen that adding electric charge only affect  
108 V<sub>d</sub> of particles in the size range of 0.2~6 μm, for which V<sub>d</sub> can be increased by up to two  
109 times. However, V<sub>d</sub> for this size range of particles are at the minimum values so the overall  
110 effect on the bulk V<sub>d</sub> of all particles should be very small. To verify this, bulk V<sub>d</sub> of PM<sub>2.5</sub> is

111 obtained by integrating the size-resolved  $V_d$  using the size-distribution assumed above. The  
112 differences in the bulk  $V_d$  between the modified ( $0.062 \text{ cm s}^{-1}$ ) and original model ( $0.06 \text{ cm}$   
113  $\text{s}^{-1}$ ) was only 3.3%.

114  
115 The size-resolved  $V_d$  from the modified model under different  $u_*$  conditions are shown in  
116 Figure 2.  $V_d$  increases with increasing  $u_*$  for all particle sizes. When  $u_*$  increased from  $0.2$  to  
117  $1.0 \text{ ms}^{-1}$  (or five times),  $V_d$  also increased by up to five times for most particle sizes. The bulk  
118  $V_d$  for  $\text{PM}_{2.5}$  shows an almost perfect linear relationship between  $V_d$  and  $u_*$  (Table 1), e.g.,  $V_d$   
119 ( $\text{cm s}^{-1}$ ) =  $0.1226 u_*$ , similar to what was found in an earlier study (Zhang and He, 2014).

120

### 121 3.2 Aerosol mass adhered to electric wire

122 Eq. (6) is used to estimate particle mass adhered to a wire accumulated during one year  
123 period ( $t = 1 \text{ year}$ ). A unit length of wire ( $L = 1 \text{ m}$ ) with a radius of  $0.5 \text{ cm}$  is chosen as the  
124 base case. A range of  $V_d$  values ( $0.025$  to  $0.122 \text{ cm s}^{-1}$ ) is applied to two different  $\text{PM}_{2.5}$   
125 concentration scenarios ( $63$  to  $121 \mu\text{g m}^{-3}$ ), which represent lower- and upper-end annual  
126 average concentrations found in the Yangtze River Delta region of China (Tao et al., 2017).  
127 Annual mass of  $\text{PM}_{2.5}$  collected by the unit-length wire is estimated to be in the range of  $1.56$   
128  $\times 10^4 \sim 1.46 \times 10^5 \mu\text{g}$ . This large range is due the large range of the estimated  $V_d$  as well as the  
129 variations in  $\text{PM}_{2.5}$  mass concentration.

130

### 131 3.3 Uncertainty analysis

132 There are many uncertainties in the above estimated aerosol mass adhered to the wire. To  
133 explore how sensitive the estimated mass to various assumed variables, sensitivity tests are  
134 conducted below on model parameters as well as environmental factors, such as considering  
135 washing off effects by rain, using higher collection efficiencies ( $E_B$  and  $E_{IM}$ ), and estimating  
136 for a different size of wire.

137  
138 Potter et al. (1991) estimated that 85% particle mass deposited to forest leaves can be washed  
139 off by rain. The percentage can be even higher for the case of wire-adsorbed particles. Using  
140 the same percentage number, the mass of  $PM_{2.5}$  adhered to an unit-length wire with a radius  
141 of 0.5 cm should then be revised to  $2.34 \times 10^3 - 2.19 \times 10^4 \mu\text{g}$  (Case 1 in Table 1).

142  
143 In equation (2), the lowest  $E_B$  and  $E_{IM}$  values over land surface (except water) were chosen  
144 for the case of wire surface assuming wire collects particles slower than any land surface by  
145 these two mechanisms. If these two values were adjusted to medium values shown in Zhang  
146 et al. (2001), the revised estimation would be in the range of  $9.30 \times 10^3 - 8.89 \times 10^4 \mu\text{g}$ , (Case  
147 2 in Table 1), which are about three times higher of the original estimation (Case 1 in table 1).

148  
149 If considering a thicker wire such as using a wire radius of 1 cm, the annual mass adhered to  
150 the wire is estimated to be in the range of  $4.68 \times 10^3 - 4.35 \times 10^4 \mu\text{g}$  (Case 3 in Table 1),  
151 basically double of those from Case 1, as is supported by from Eq. (6).

152

#### 153 **4. Conclusions**



154 Under typical aerosol pollution conditions in the Yangtze River Delta region of China,  
155 particle mass collected by and adhered to high-voltage electric wires are estimated to be on  
156 the order of  $10^3$ - $10^4$   $\mu\text{g}$  per unit length (1 m) wire during one year period. These numbers  
157 could be used as a first estimation for studying aerosol deposition impact on electric wire  
158 related issues, keeping in mind that such estimation does not include contributions from fog,  
159 humid, or icy conditions when aerosol deposition might be substantially enhanced. Future  
160 studies may focus on chemically resolved particle mass deposited on wires since it is the  
161 charged ions that may have the strongest negative impact on insulators, as well as introduce  
162 the deposition scheme into a 3-D air quality model.

163  
164 This study provides a first estimation of particle mass collected by electric wires, although  
165 with large uncertainties in physical and chemical physical interaction between aerosols and  
166 wire surface, which can be used for subsequent impact studies of aerosol pollution on  
167 electricity transfer. Air pollution flashover caused by long-term dust contamination mainly  
168 takes place on dirty insulators rather than on power lines which have more simple shape  
169 compared to complex shapes of insulators, which could be a further study.

170  
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Table 1. The modeled bulk  $V_d$  of  $PM_{2.5}$  under five different  $u_*$  conditions and estimated  $PM_{2.5}$  mass adhered to unit-length wire (1 m) during one year period under five different  $u_*$  and two different  $PM_{2.5}$  concentration scenarios.

$u_*$ ( $m\ s^{-1}$ )	0.2	0.4	0.6	0.8	1.0
$V_d$ ( $cm\ s^{-1}$ )	0.025	0.05	0.074	0.098	0.122
Particle mas - Base case					
$PM_{2.5}$ ( $63\ \mu g\ m^{-3}$ )	$1.56 \times 10^4$	$3.12 \times 10^4$	$4.62 \times 10^4$	$6.11 \times 10^4$	$7.61 \times 10^4$
$PM_{2.5}$ ( $121\ \mu g\ m^{-3}$ )	$3.00 \times 10^4$	$5.99 \times 10^4$	$8.87 \times 10^4$	$1.17 \times 10^5$	$1.46 \times 10^5$
Particle mass – Case 1 (Base case plus washed off effect by rain)					
$PM_{2.5}$ ( $63\ \mu g\ m^{-3}$ )	$2.34 \times 10^3$	$4.68 \times 10^3$	$6.92 \times 10^3$	$9.17 \times 10^3$	$1.14 \times 10^4$
$PM_{2.5}$ ( $121\ \mu g\ m^{-3}$ )	$4.49 \times 10^3$	$8.99 \times 10^3$	$1.33 \times 10^4$	$1.76 \times 10^4$	$2.19 \times 10^4$
Particle mass – Case 2 (Case 1 plus adjusted $E_B$ and $E_{IM}$ )					
$PM_{2.5}$ ( $63\ \mu g\ m^{-3}$ )	$9.30 \times 10^3$	$1.85 \times 10^4$	$2.78 \times 10^4$	$3.69 \times 10^4$	$4.64 \times 10^4$
$PM_{2.5}$ ( $121\ \mu g\ m^{-3}$ )	$1.79 \times 10^4$	$3.56 \times 10^4$	$5.33 \times 10^4$	$7.10 \times 10^4$	$8.89 \times 10^4$
Particle mass – Case 3 (Case 1 plus wire radius of 1.0 cm)					
$PM_{2.5}$ ( $63\ \mu g\ m^{-3}$ )	$4.68 \times 10^3$	$9.17 \times 10^3$	$1.37 \times 10^4$	$1.82 \times 10^4$	$2.26 \times 10^4$
$PM_{2.5}$ ( $121\ \mu g\ m^{-3}$ )	$8.99 \times 10^3$	$1.76 \times 10^4$	$2.62 \times 10^4$	$3.49 \times 10^4$	$4.35 \times 10^4$

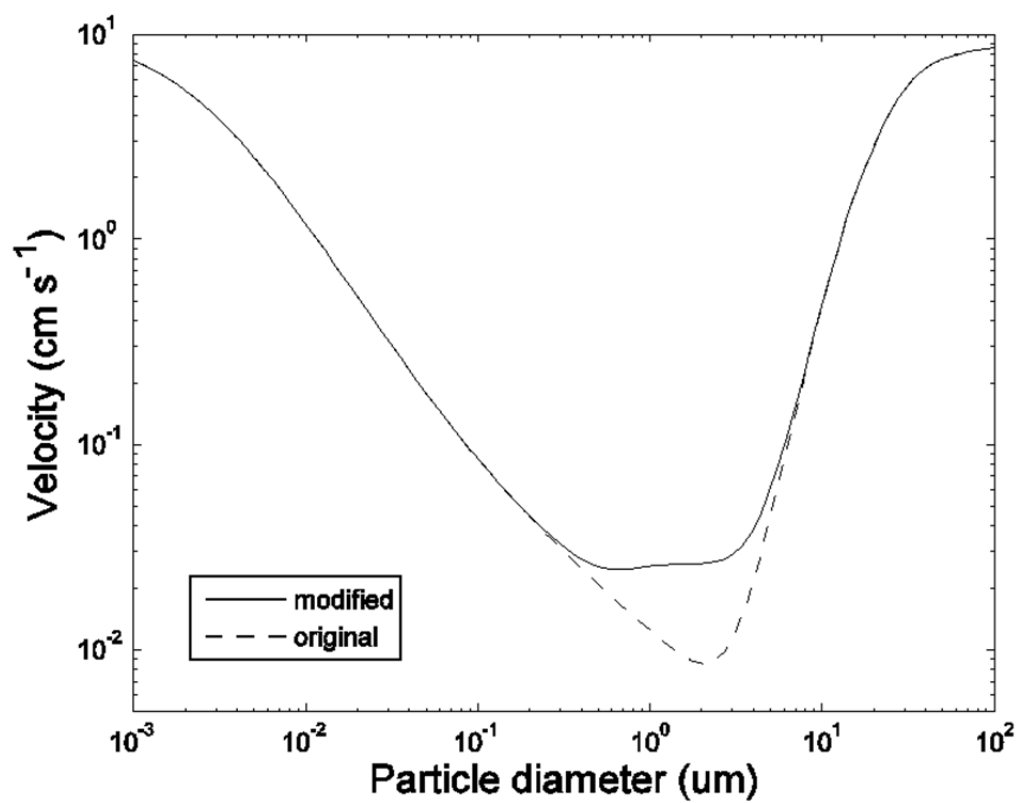


Figure1. Size-resolved  $V_d$  from the modified and the original models.

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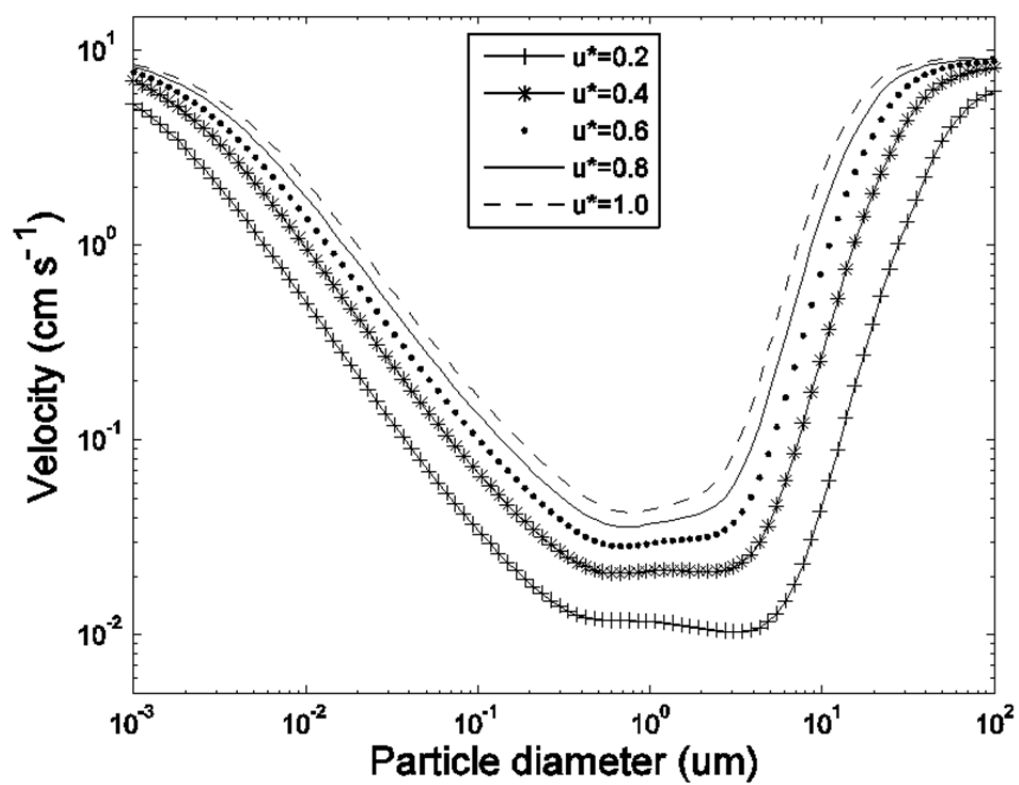


Figure2. Modeled size-resolved  $V_d$  under different  $u^*$  conditions.